

## Acting Manager:

Dr. Mohammad Khansari  
Assistant Professor  
ICT Research Institute

## Editor - In - Chief:

Dr. Kambiz Badie  
Associate Professor  
ICT Research Institute

## Executive Manager:

Prof. Ahmad Khadem-Zadeh  
Associate Professor  
ICT Research Institute

## Associate Editor (CT Section):

Dr. Reza Faraji-Dana  
Professor  
University of Tehran

## Associate Editor (Network Section):

Dr. S. Majid Noorhoseini  
Assistant Professor  
Amirkabir University of Technology

## Editorial Board:

Dr. Prof. Abdolali Abdipour  
Professor  
Amirkabir University of Technology

Dr. Hassan Aghaeinia  
Associate Professor  
Amirkabir University of Technology

Dr. Vahid Ahmadi  
Professor  
Tarbiat Modares University

Dr. Abbas Asosheh  
Assistant Professor  
Tarbiat Modares University

Dr. Karim Faez  
Professor  
Amirkabir University of Technology

Dr. Hossein Gharaie  
Assistant Professor  
ICT Research Institute

Dr. Farrokh Hodjat Kashani  
Professor  
Iran University of Science & Technology

Dr. Ehsanollah Kabir  
Professor  
Tarbiat Modares University

Dr. Mahmoud Kamarei  
Professor  
University of Tehran

Dr. Manouchehr Kamyab  
Associate Professor  
K. N. Toosi University of Technology

Dr. Ghasem Mirjalili  
Associate Professor  
Yazd University

Dr. Kamal Mohamed-pour  
Professor  
K.N. Toosi University of Technology

Dr. Ali Moini  
Associate Professor  
University of Tehran

Dr. Ali Movaghar Rahimabadi  
Professor  
Sharif University of Technology

Dr. Keyvan Navi  
Associate Professor  
Shahid Beheshti University

Dr. Jalil Rashed Mohasel  
Professor  
University of Tehran

Dr. Babak Sadeghian  
Associate Professor  
Amirkabir University of Technology

Dr. S. Mostafa Safavi Hemami  
Associate Professor  
Amirkabir University of Technology

Dr. Ahmad Salahi  
Associate Professor  
ICT Research Institute

Dr. Hamid Soltanian-Zadeh  
Professor  
University of Tehran

Dr. Fattaneh Teghiyareh  
Assistant Professor  
University of Tehran

Dr. Mohammad Teshnehlab  
Associate Professor  
K. N. Toosi University of Technology

Dr. Mohammad Hossein Yaghmaee Moghaddam  
Associate Professor  
Ferdowsi University of Mashhad

Dr. Alireza Yari  
Assistant Professor  
ICT Research Institute

## Secretariat Organizer:

Taha Sarhangi

## Executive Assistants:

Valiollah Ghorbani  
Nayereh Parsa-Shirin Mirzaie Ghazi



**Topics of Interest**

**Information Technology**

Information Systems

IT Applications & Services

IT Platforms: Software & Hardware Technology

IT Strategies & Frameworks

**Communication Technology**

Communication Devices

Communication Theory

Mobile Communications

Optical Communications

Satellite Communications

Signal / Image / Video Processing

**Network Technology**

Computer & Communication Networks

Wireless Networks

Network Management

Network Security

NGN Technology

Security Management

IJICTR

This Page intentionally left blank.



## *Gain and Bandwidth Enhancement of Slot Antenna Using Two Unprinted Dielectric Superstrate*

Rasoul Fakhte

Electrical Engineering Department  
University of Guilan  
Rasht, Iran  
rasoul\_fa@yahoo.com

Habib Ghorbaninejad

Electrical Engineering Department  
University of Guilan  
Rasht, Iran  
ghorbaninejad@guilan.ac.ir

Received: April 17, 2016- Accepted: July 23, 2016

**Abstract**— This paper presents a high-gain and wideband antenna with a compact, simple and low-profile structure. The design strategy of high gain Fabry-Perot resonator antennas (FPRA), which have a superstrate with increasing phase in the operating band, has been applied to design the antenna. A double-layered unprinted dielectric superstrate is used as a partially reflective surface (PRS) to enhance the gain of the antenna and to produce a reflection phase curve versus frequency with a positive slope. The superstrate is composed of two dielectric slabs, and it is truncated so that its dimension to be about  $1.5\lambda \times 1.5\lambda$ . By using such an unprinted double-layered dielectric, as a superstrate, the bandwidth of about 14.3% can be achieved. To further increase the size of the upper unprinted slab, the gain can be enhanced, without compromising the bandwidth. A prototype antenna has been designed and simulated at 9 GHz. The achieved peak gain is 17 dB.

**Keywords**- Cavity antenna, Fabry-Perot antenna, Superstrate, High gain.

### I. INTRODUCTION

The gain of a small antenna such as a patch, dipole or slot, can be enhanced by using a partially reflecting superstrate (PRS). This idea first introduced by Trentini in 1956 [1] and later investigated by Jackson and Alexopoulos in 1985 [2]. Antennas of this nature utilize a resonant cavity formed between a conducting ground plane and the PRS. The excited fields in the cavity undergo multiple reflections at resonance and leak through the PRS in broadside direction as a highly directive beam. Such antennas are known as resonant cavity antennas, two dimensional leaky-

wave antennas or Fabry-Pérot resonator antennas. With a planar configuration and simple design, these antennas are considered as a potential replacement for bulkier high-gain antennas, such as horns or reflectors, for a number of exciting applications. Typically, a PRS with high permittivity or high permeability ( $\epsilon \gg 1$  or  $\mu \gg 1$ ) material [2] and a large area [3, 4] is used to achieve strong superstrate reflectivity [5]. The Fabry-Perot cavity antennas are obviously cavity antennas that have been studied for a long time in the microwave community. The Fabry-Perot resonator antenna is a kind of highly directive antenna [5], which is formed by placing a partially



reflective surface (PRS) in front of a simple primary radiator with a ground plane. Several applications have been proposed for similar structures such as antennas with the required phase-front and amplitude linearity for helicopter stabilization [6] or tracking systems for missiles [7]. An exhaustive source about the theory, design and practical applications of the cavity-type antennas can be found in [8]. Recently, it has been proposed to design cavity antennas with no uniform mirrors to obtain very low side lobes [9]. More recently, Fabry-Perot resonator antennas (FPRAs) attract researcher's attention [10-14], due to their advantages of high gain; simplicity, low cost, etc. Recently, a new waveguide slot antenna has been proposed that considerably improve the antenna specifications using radiating surface [15]. Also, in [16] a thick unprinted dielectric slab of quarter-wavelength is located above a slot antenna to achieve concurrently high gain and large bandwidth. In [17] a wideband resonant cavity antenna (RCA) with circular polarization has been proposed with high-gain performance. The main beam of a Fabry-Perot cavity antenna produces side-lobes which are proportional to the scan angle. An alternative mechanism using dielectric-ferrite superstrate has been proposed to control side-lobe level [18]. In this paper two simple unprinted dielectric slabs with the same side dimensions and different thickness have been used as superstrate to improve the antenna gain and bandwidth, over a wide frequency band, so that, a slotted antenna which is excited by a rectangular waveguide, has been used as the primary radiating source.

II. ANTENNA DESIGN

The configuration of the proposed high-gain slot antenna is shown in Fig. 1. The superstrate is composed of two square dielectric slabs which have same side lengths of  $d$  and thickness of  $t_1$  and  $t_2$ . The lower superstrate is symmetrically placed above the slot plane (as the ground plane) at a given height. There is an air gap between the two slabs, whose height is  $h_2$ . Each dielectric layer is assumed lossless, homogeneous, and isotropic. A Fabry-Perot cavity is formed by the superstrate and a PEC ground (slot plane). The separation area between the PEC and the superstrate is considered free space and the height is  $h_1$ .

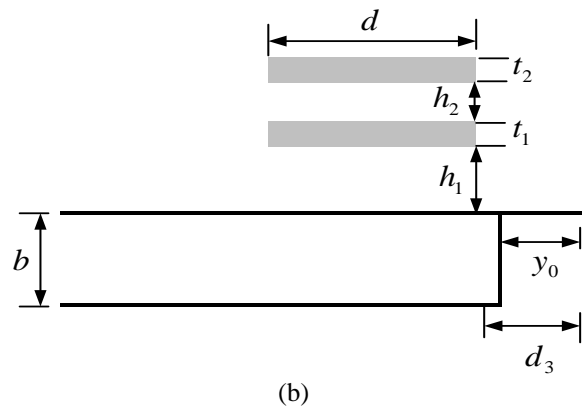
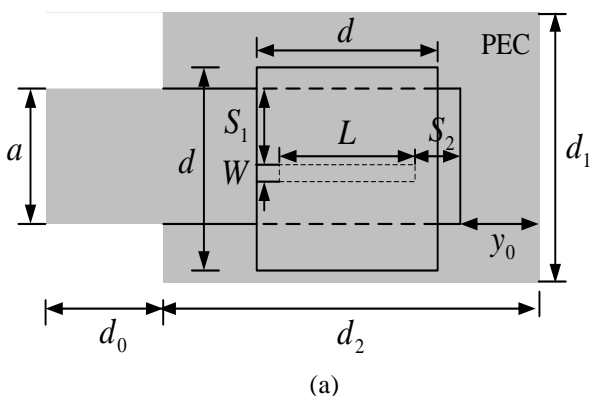


Fig. 1. Configuration of the proposed waveguide slot antenna (a) Top view (b) Side view

A rectangular waveguide WR90 is used to feed the Fabry-Perot Cavity Antenna. A rectangular slot was made in a 1 mm-thick copper ground plane and dimensions of slot are:  $L=18$  mm and  $W=3.5$  mm. The design of the antenna starts from that of the superstrate or partially reflective surface. As demonstrated in [10], a superstrate with increasing phase inside the operating band might lead to a wideband Fabry-Perot resonator antenna. According to the ray-tracing analysis in [1], the reflection phase of the PRS required for maximum broadside radiation at the resonance frequency can be formulated as

$$\rho_H = \frac{4\pi h}{c} f + (2N - 1)\pi \tag{1}$$

Where  $h$  is the cavity thickness,  $f$  is the operating frequency,  $N=1, 2, \dots$  is an integer number and  $c$  is the light velocity in free space. If reflection coefficient of the superstrate is  $\rho \exp(j\psi)$  and  $f(\alpha)$  is the normalized field pattern of feed antenna, then normalized electric field  $E$  and power  $S$  at an angle  $\alpha$  to the normal is derived in [10].

$$|E| = \sqrt{\frac{1-\rho^2}{1+\rho^2-2\rho\cos\phi}} f(\alpha), \quad s = \frac{1-\rho^2}{1+\rho^2-2\rho\cos\phi} f^2(\alpha) \tag{2}$$

Where,  $\phi$  is the phase difference between waves reflecting from PRS. Bore sight gain ( $\theta=0^\circ$ ) and bandwidth is function of reflection coefficient [1]:

$$G = \frac{1+\rho}{1-\rho} \quad BW = \frac{\Delta f}{f_0} = \left( \frac{\lambda}{2\pi l_r} \right) \frac{1-\rho}{\rho^{0.5}} \tag{3}$$

For the waves reflecting from PRS to be in phase in normal direction, resonant distance  $L_r$  between ground plane and PRS is given by [1].

$$L_r = \left( \frac{\psi_0}{360} - 0.5 \right) \frac{\lambda}{2} + N \frac{\lambda}{2} \tag{4}$$

Where  $\psi_0$  is phase angle of reflection coefficient of the PRS in degree and  $N$  is a non-negative integer number.

The design frequency band in this work is considered to be in frequency range of 8.4-9.7 GHz. In the design procedure (which will be explained in detail by parametric study in this section), the permittivity of two slabs is chosen to be  $\epsilon_1=6.15$  (lower slab) and  $\epsilon_2=2.2$  (upper slab). The thicknesses of slabs are 2.916 mm and 5.5 mm, respectively, and parameter  $h_2$  is 6.2 mm. Fig. 2 and Fig. 3 shows the reflection magnitude and the gain of the proposed antenna with and without PRS (conventional one), respectively. The peak gain is about 17 dBi.



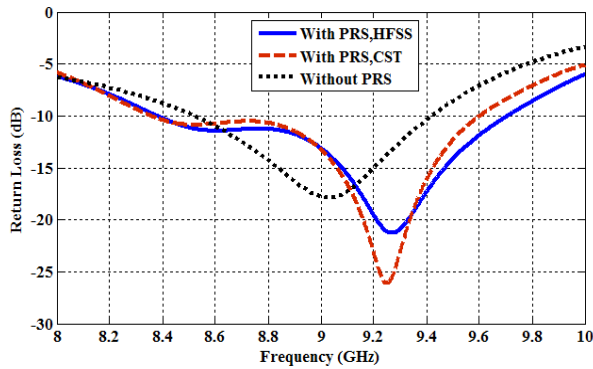


Fig. 2 Simulated return loss of the proposed waveguide slot antenna compared with conventional one. Proposed antenna:  $a=22.86$  mm,  $b=10.16$  mm,  $d_0=20$  mm,  $d_1=95$  mm,  $d_2=67.5$  mm,  $d_3=33.72$  mm,  $y_0=30$  mm,  $L=18$  mm,  $W=3.5$  mm,  $S_1=1.68$  mm,  $S_2=3.72$  mm,  $d=50$  mm,  $h_1=19.4$  mm,  $h_2=6.2$  mm,  $t_1=2.91$  mm,  $t_2=5.5$  mm.

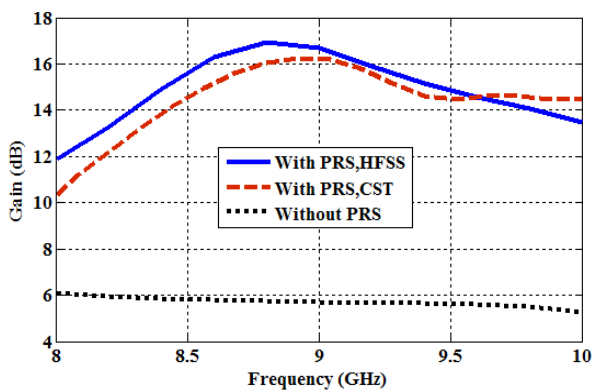


Fig. 3 Simulated gain of proposed waveguide slot antenna compared with conventional one.

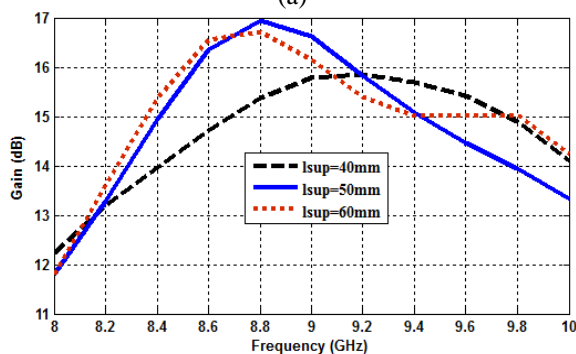
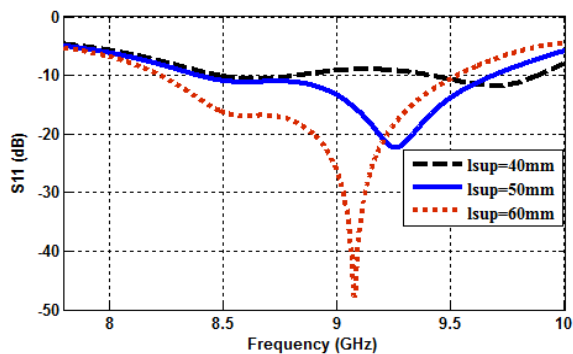


Fig. 4 Return loss and gain of the proposed antenna for a set of superstrate length values

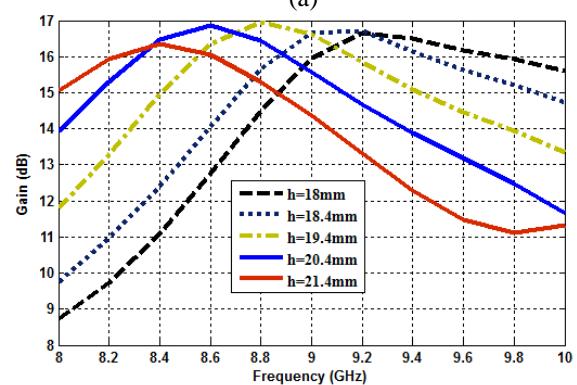
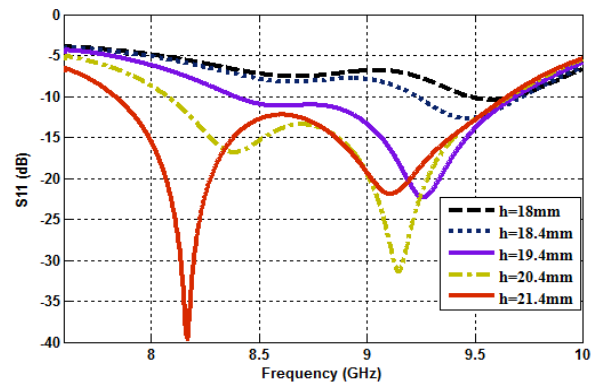
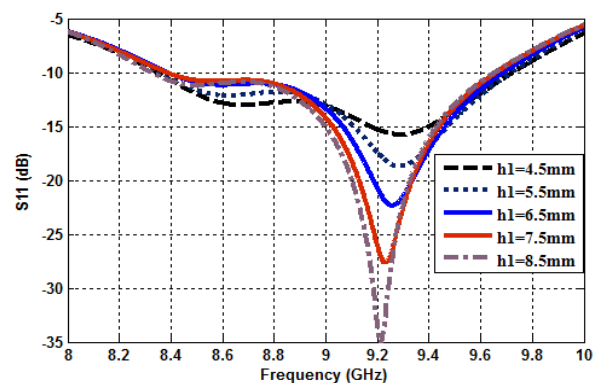


Fig. 5. The return loss and the gain of the proposed antenna for a set of superstrate height values. (a) Return loss (b) Gain.

Fig. 4 shows the return loss and the gain of the proposed antenna, for a set number of superstrate length values.

It has been shown in Fig. 4 that antenna bandwidth can be approximately enhanced by reducing the size of the PRS [11, 14]. It also can be found that the gain will decrease while the antenna bandwidth will increase with decreasing the size of PRS. The designed FPRA has been used to study the relation of the bandwidth and the directivity by gradually reducing the size of the PRS. The designed PRS is applied to form a FPRA. Apparently, a wideband high-gain FPRA is obtained. It was also found that the optimum gain and the bandwidth are obtained when the size of the square slabs is about  $1.5\lambda \times 1.5\lambda$ .

Fig. 5 shows the return loss and the gain of the proposed antenna, for a set number of superstrate height values.



(a)



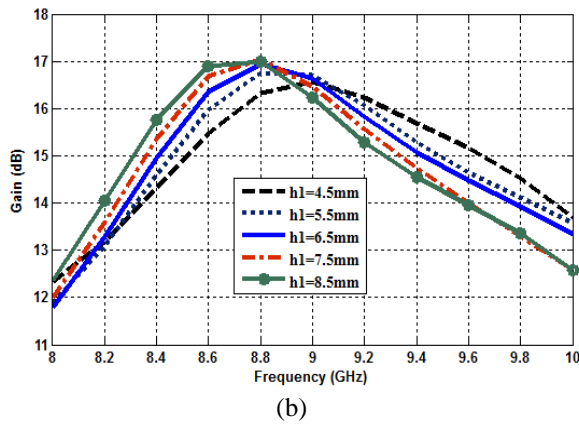


Fig. 6. Return loss and gain of the proposed antenna for different values of space between PRSs (a) Return loss (b) Gain.

Fig. 5 depicts that antenna bandwidth can be significantly enhanced by increasing the size of the PRSs. It also can be found that the antenna peak gain shifted to lower frequency with increasing the superstrate height. As it is observed from Fig. 5 (a), parameter  $h$ , has more effect on the first resonant frequency compared to the second one that confirms the fact that the first resonant frequency (8.2 GHz) is related to cavity and second resonance frequency due to slot.

Fig. 6 shows the return loss and the gain of the proposed antenna for different values of space between PRSs. It shows that by increasing the distance between dielectrics, the gain slightly increased, but to achieve compact size, the distance between the dielectric is selected to be  $h_1 = 6.5$  mm. Fig. 7 shows the effects of the extended broad wall size of the antenna (ground size) on the antenna peak gain.

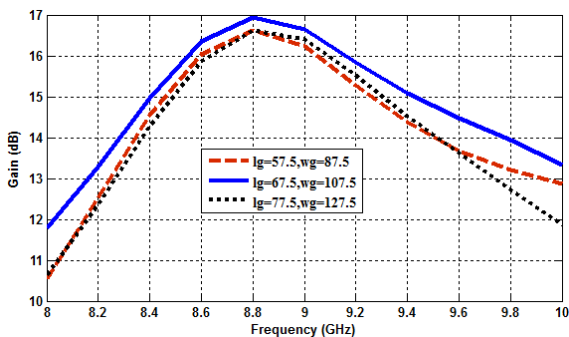


Fig. 7. Effects of ground size on the proposed antenna gain.

As it can be seen from Fig. 7 for  $l_g = d_2 = 67.5$  mm,  $w_g = d_1 = 107.5$  mm, the proposed antenna has maximum gain. Fig. 8 shows the return loss and the gain of the proposed antenna for different dielectric constant of PRS 1 (lower PRS).

As can be seen from Fig. 8, although antenna bandwidth slightly increased with increasing in dielectric constant but for  $\epsilon_1 = 6.15$ , the proposed antenna has maximum gain, so, dielectric constant for lower PRS is selected to be 6.15.

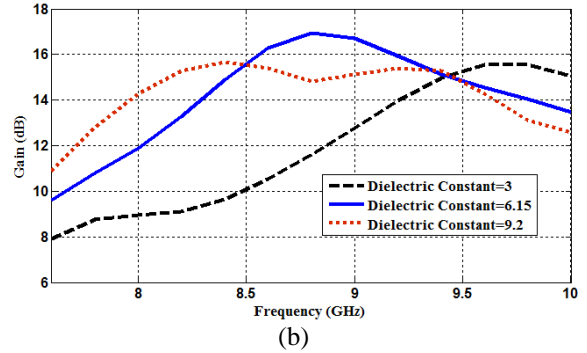
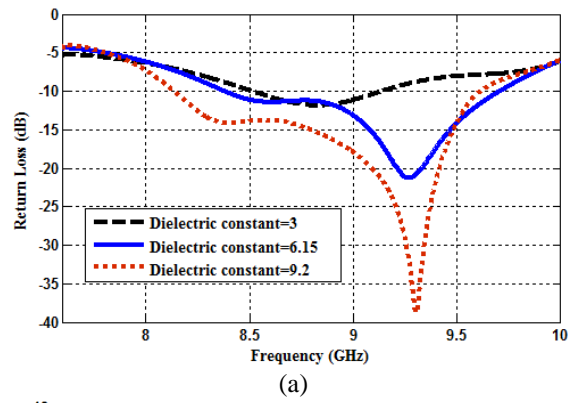


Fig. 8. Effects of PRS 1 various dielectric constant on the proposed antenna (a) Return loss (b) Gain.

Fig. 9 shows the effects of PRS2 with various dielectric constants on the proposed antenna. As can

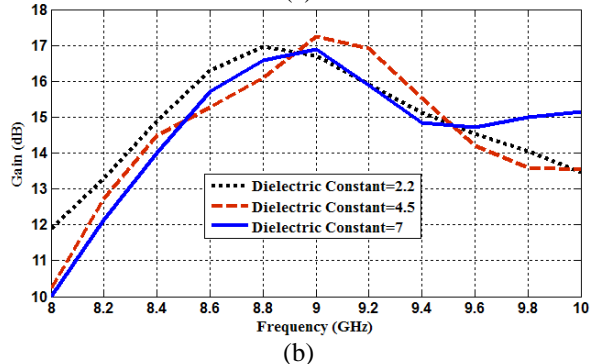
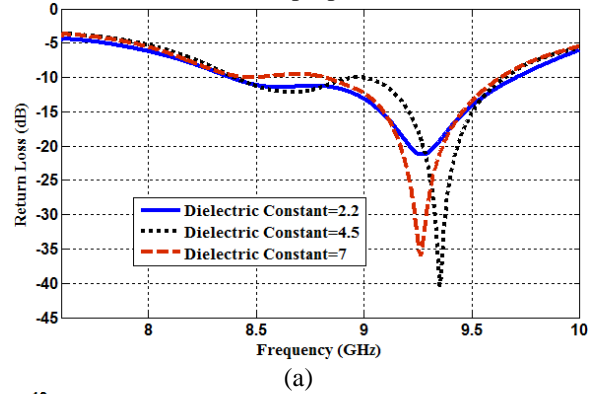


Fig. 9. Effects of PRS 2 with various dielectric constants on the proposed antenna (a).return loss (b). Gain.

be seen from Fig. 9 bandwidth and gain of the proposed antenna for different dielectric constants of PRS 2, is same, therefore considering the price and ease of preparation, dielectric constant for PRS2 is selected 2.2. The radiation patterns of the antenna in the E- and H-planes at three different frequencies, within its bandwidth, are shown in Fig. 10. It is noted



that the side lobe levels are below  $-10$  dB from 8.6 to 9.3 GHz and tend to increase above  $-10$  dB as the frequency increases.

In the antenna design, the size of the two slabs are  $50\text{mm} \times 50\text{mm} \times 2.916\text{mm}$  and  $50\text{mm} \times 50\text{mm} \times 5.5\text{mm}$ , respectively. The heights ( $h_1$  and  $h_2$ ) of two air gaps are  $19.4\text{mm}$  and  $6.2\text{mm}$ , respectively. The size of the ground is  $67.5\text{mm} \times 95\text{mm}$ .

Fig. 11. depicts the radiation efficiency of the proposed antenna that is over 98%.

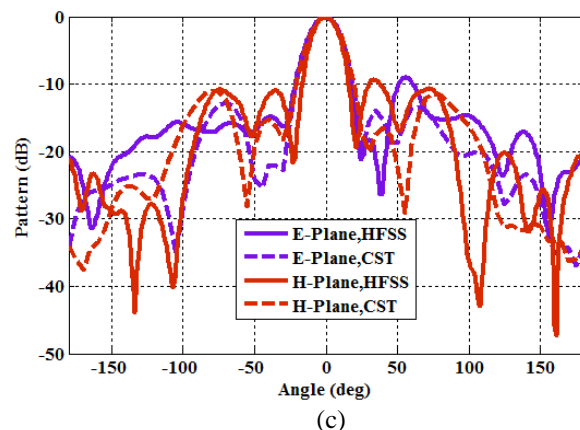
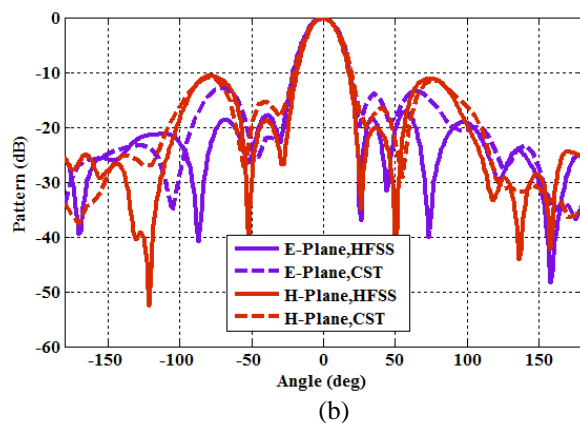
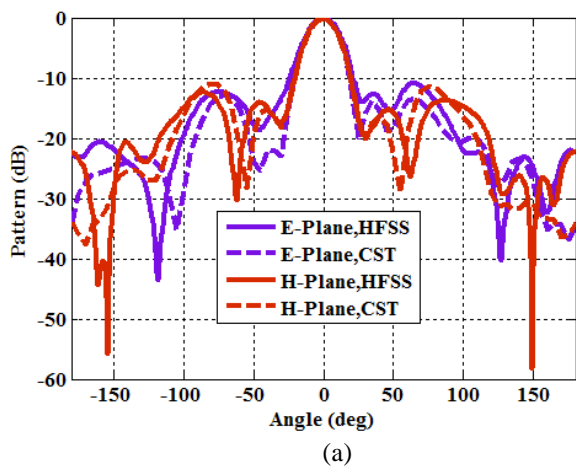


Fig. 10. Radiation patterns of antenna: (a) 8.6 GHz, (b) 9 GHz, (c) 9.3 GHz

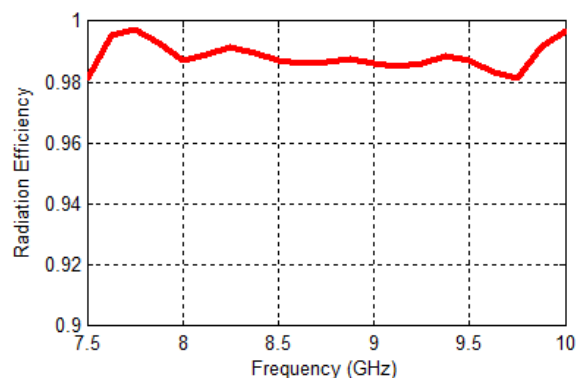


Fig. 11. Radiation efficiency of the proposed antenna

### III. CONCLUSION

The proposed antenna is designed to verify its high gain performance. Commercial software HFSS is used to carry out the simulations. The antenna consists of a PEC ground, a PRS, which is composed of two slabs with different thickness, permittivity, and a feed. The simulated good impedance matching, determined by  $|S_{11}| < -10$  dB, is obtained from 8.4 GHz to 9.7 GHz. The gain of the slot antenna is enhanced over a wide-frequency band validating the feasibility of using a simple PRS with small area.

### REFERENCES

- [1] Trentini, G.V.: 'Partially reflecting sheet arrays', IRE Trans. Antennas Propag., vol. 4, pp. 666-671, 1956.
- [2] Jackson, D.R., and Alexopoulos, N.G.: 'Gain enhancement methods for printed circuit antennas', IEEE Trans. Antennas Propag., vol. 33, No.9, pp. 976-987, 1985.
- [3] Cheyde, C., Serier, C., Thevenot, M., Monediere, T., Reineix, A., and Jecko, B.: 'An electromagnetic bandgap resonator antenna', IEEE Trans. Antennas Propag., Vol. 50, No. 9, pp. 1285-1290, 2002.
- [4] Weily, A.R., Esselle, K.P., Bird, T.S., and Sanders, B.C.: 'High-gain 1D EBG resonator antenna', Microw. Opt. Lett., Vol. 47, No. 2, pp. 107-114, 2005.
- [5] Feresidis, A.P., and Vardaxoglou, J.C.: 'High gain planar antenna using optimised partially reflective surfaces', IET Microw. Antennas Propag., Vol. 148, No. 6, pp. 345-350, 2001.
- [6] P. J. Klass, "Helicopter stabilized by microwave beam," Aviation Week and Space Technol., vol. 79, pp. 85-89, 1968.
- [7] E. C. Belee, R. C. Breithaupt, D. L. Godwin, and S. H. Walker, "Image element antenna array for a monopulse tracking system for a missile," U.S. Patent 3 990 078, Nov. 2, 1976.
- [8] A. Kumar and H. D. Hristov, Microwave Cavity Antennas. New York: Artech House, 1989.
- [9] R. Sauleau, P. Coquet, T. Matsui, and J.-P. Daniel, "A new concept of focusing antennas using plane-parallel Fabry-Perot cavities with nonuniform mirrors," IEEE Trans. Antennas Propag., vol. 51, no. 11, pp. 3171-3175, Nov. 2003.
- [10] Y. Ge, K. P. Esselle, and Trevor Bird, "The Use of Simple Thin Partially Reflective Surfaces with Positive Reflection Phase Gradients to Design Wideband, Low-Profile EBG Resonator Antennas", IEEE Trans. Antennas Propag., vol. AP-64, no. 2, pp. 743 - 750, Feb. 2012
- [11] Yuehe Ge, Can Wang and Xiaohu Zeng, "Wideband High-Gain LowProfile 1D Fabry-Perot Resonator Antennas", 2013 International Symposium on Antennas and Propagation (ISAP2013), Nanjing, China, Oct. 23 - 25, 2013.





- [12] Y. Ge, K.P. Esselle, and T.S. Bird, "A method to design dual-band, high-directivity EBG resonator antennas using single-resonant, single-layer partially reflective surface", *Progress in Electromagnetic Research C*, vol. 13, pp. 245 – 257, 2010.
- [13] B. A. Zeb, Y. Ge, K. P. Esselle, Z. Sun, and M. E. Tobar, "Dual-Band High Gain 1-D Electromagnetic Band Gap (EBG) Resonator Antenna Design using Enhanced Reflection Phase Gradient", *IEEE Trans. Antennas Propag.*, vol. AP-64, no. 10, pp. 4522 - 4529, Oct. 2012.
- [14] Lee, Young Ju, et al "Application of electromagnetic band-gap (EBG) superstrates with controllable defects for a class of patch antennas as spatial angular filters." *IEEE Transactions on Antennas and Propagation* 53.1 (2005): 224-235.
- [15] Fakhte, Rasoul, and Habib Ghorbaninejad. "High gain and improved waveguide slot antenna using a metallic superstrate as main radiator." *IET Microwaves, Antennas & Propagation* (2016).
- [16] Zeb, B. A., R. M. Hashmi, and K. P. Esselle. "Wideband gain enhancement of slot antenna using one unprinted dielectric superstrate." *Electronics Letters* 51.15 (2015): 1146-1148.
- [17] Tran, Huy Hung, and Ikmo Park. "Compact wideband circularly polarised resonant cavity antenna using a single dielectric superstrate." *IET Microwaves, Antennas & Propagation* 10.7 (2016): 729-736.
- [18] Sultan, Farooq, and Sheikh Sharif Iqbal Mitu. "Superstrate-Based Beam Scanning of a Fabry–Perot Cavity Antenna." *IEEE Antennas and Wireless Propagation Letters* 15 (2016): 1187-1190.



**R. Fakhte** was born in Guilan, Iran. He received his B.Sc. degree in Electrical Engineering and his M.Sc. degree in Telecommunication Engineering from University of Guilan in 2016. His scientific field of interest is design and analysis of high gain antenna and wireless components.



**H. Ghorbaninejad-Foumani** was born in Guilan, Iran. He received his B.Sc. degree from University of Guilan in 2003 and his M.Sc. and Ph.D. degrees from Iran University of Science and Technology (IUST) in 2005 and 2010 respectively, all in Telecommunication Engineering. He is currently assistant professor at department of electrical engineering of University of Guilan. His scientific fields of interest are electromagnetic problems including microwave and spatial filter design, compact microwave devices and finding Green's function of microwave structures.

